

bladio Primo N.2

COMUNE DI GENOVA  
RIPARTIZIONE EDILIZIA COMUNALE  
SCUOLA MEDIA STRATALE "G. PARINELLI"

CALCOLO TRAVI 1° SOLAIO

284 30.11.1979

*[Signature]*

- REAZIONI -										- Reazioni Travi -																								
Tr.	l.n.	le	Polo Repart.	Nucleo Perim.	Tramete	Polite Repart.	Polo Repart.	(p)	IP	Coef. Numer. Fiss.	Mf. kg. cm.	b cm.	$\sqrt{\frac{M}{b}}$ cm.	H cm.	$\frac{b}{H}$ cm.	$\beta$	$\alpha$ kg/cm.	$\alpha f$ kg/cm.	$\alpha$ cm.	$\frac{\alpha}{\beta}$ cm.	$T_f = \beta b \sqrt{\frac{M}{b}}$ cm <sup>2</sup>	ARMATURA	T	b <sub>0</sub>	$\frac{b}{\sqrt{b}}$ cm.	$\frac{b}{\sqrt{b}}$ cm.	c	SH.	Sfp	Sf = SH-Sfp	$\alpha$	Stile	Altezza	
P1	210	220	140	400	-	2060	-	2900	6.100	3.050	3.050	1/12	112.000	25	67	40	36	0.537	0.125	38	1600	$0.141 \times 141 \times 141 = 210$	2φ10 + 2φ8	3.050	14	32	470	6.80	$0.141 \times 141 \times 141 = 210$	2φ8 = 1.01	2.80	0.57	5	10φ6
P2	210	220	140	400	-	2060	-	2900	6.100	3.050	3.050	1/12	112.000	25	67	40	36	0.537	0.125	38	1600	$0.141 \times 141 \times 141 = 210$	2φ10	3.050	14	32	470	6.80	$0.141 \times 141 \times 141 = 210$	2φ10 = 1.57	4.93	1.01	5	10φ8
P3	300	315	250	1100	-	2580	-	3930	11.800	5.900	5.900	1/10	372.000	35	108	50	46	0.426	0.159	50	1600	$0.159 \times 159 \times 159 = 365$	4φ14	5.900	16	40	640	9.30	$0.159 \times 159 \times 159 = 365$	2φ14 = 3.08	5.32	0.57	9.5	19φ6
P4	290	305	250	1100	-	2580	-	3930	11.800	5.900	5.900	1/12	290.000	35	91	50	46	0.384	0.133	41	1600	$0.133 \times 133 \times 133 = 425$	2φ14 + 2φ10	5.900	16	40	640	9.30	$0.133 \times 133 \times 133 = 425$	2φ10 = 1.57	6.33	1.01	6.5	13φ8
P5	218	225	150	680	-	-	-	830	1.800	900	900	1/10	41.000	25	405	24	21	0.577	0.189	40	1600	$0.129 \times 129 \times 129 = 135$	3φ10	900	25	19	475	2.00	$0.129 \times 129 \times 129 = 135$	1φ8 = 0.79	1.31	0.57	3	6φ6
P6	340	355	180	680	-	-	-	830	2.800	1400	1400	1/10	100.000	35	53	24	21	0.400	0.170	50	1600	$0.170 \times 170 \times 170 = 5$	3φ10	1400	35	19	475	2.00	$0.170 \times 170 \times 170 = 5$	2φ10 = 1.57	3.33	0.57	6.5	13φ6
P7	218	225	150	680	-	-	-	830	1.800	900	900	1/10	41.000	25	405	24	21	0.577	0.189	40	1600	$0.170 \times 170 \times 170 = 5$	3φ10	1400	35	19	475	2.00	$0.170 \times 170 \times 170 = 5$	2φ10 = 1.57	3.33	0.57	6.5	13φ6
P8	340	355	180	680	-	-	-	830	2.800	1400	1400	1/10	100.000	35	53	24	21	0.400	0.170	50	1600	$0.170 \times 170 \times 170 = 5$	3φ10	1400	35	19	475	2.00	$0.170 \times 170 \times 170 = 5$	2φ10 = 1.57	3.33	0.57	6.5	13φ6
P9	140	150	150	1100	-	-	-	1250	1.750	875	875	1/10	80.000	35	655	40	36	0.476	0.145	44	1600	$0.141 \times 141 \times 141 = 375$	2φ12 + 2φ10	4.100	16	32	510	8.10	$0.141 \times 141 \times 141 = 375$	2φ10 = 1.57	4.23	0.57	7.5	15φ6
P10	235	245	200	1100	-	2200	-	3500	8.200	4.100	4.100	1/10	240.000	35	88.6	40	36	0.431	0.157	49.5	1600	$0.157 \times 157 \times 157 = 412$	3φ12 + 1φ14	4.900	16	32	510	8.10	$0.157 \times 157 \times 157 = 412$	1φ12 + 1φ14 = 2.67	5.60	1.01	6	12φ8
P11	280	300	200	1100	-	2200	-	3500	9.800	4.900	4.900	1/12	245.000	35	88.6	40	36	0.431	0.157	49.5	1600	$0.157 \times 157 \times 157 = 412$	3φ10	780	16	32	510	2.00	$0.157 \times 157 \times 157 = 412$	1φ10 = 0.79	2.01	0.57	3.5	11φ6
P12	222	235	200	250	-	250	-	700	1.560	780	780	1/12	31.000	25	38	40	36	1.000	0.067	20	1100	$0.067 \times 67 \times 67 = 0.60$	3φ10	1700	16	32	510	3.40	$0.067 \times 67 \times 67 = 0.60$	2φ12 = 2.26	4.30	0.57	8	16φ6
P13	270	285	200	800	-	250	-	1250	3.400	1700	1700	1/12	81.000	25	58	40	36	0.650	0.107	32.5	1600	$0.107 \times 107 \times 107 = 1.56$	3φ10	1700	16	32	510	3.40	$0.107 \times 107 \times 107 = 1.56$	2φ12 = 2.26	4.30	0.57	8	16φ6
P14	425	440	200	800	-	250	-	1250	5.300	2650	2650	1/10	234.000	35	82	40	36	0.439	0.157	48.6	1600	$0.157 \times 157 \times 157 = 412$	4φ12	2650	16	32	510	5.30	$0.157 \times 157 \times 157 = 412$	2φ12 = 2.26	7.21	0.57	12.5	25φ6
P15	430	450	300	800	-	1940	-	3040	13.100	6470	6470	1/10	570.000	40	121	60	56	0.460	0.107	46	1600	$0.107 \times 107 \times 107 = 1.56$	2φ16 + 3φ12	6.570	20	50	1.000	6.57	$0.107 \times 107 \times 107 = 1.56$	3φ12 = 3.39	7.21	0.57	12.5	25φ6
P16	430	450	300	800	-	1940	-	3040	13.100	6470	6470	1/10	570.000	40	121	60	56	0.460	0.107	46	1600	$0.107 \times 107 \times 107 = 1.56$	2φ16 + 3φ12	6.570	20	50	1.000	6.57	$0.107 \times 107 \times 107 = 1.56$	3φ12 = 3.39	7.21	0.57	12.5	25φ6
P17	340	355	380	1.100	-	1800	-	1480	5.000	3.170 + 2.300 = 5.470	3.170 + 2.300 = 5.470	1/10	178.000	40	121	60	60	0.445	0.135	42	1600	$0.135 \times 135 \times 135 = 2.60$	3φ14 + 2φ12	5.470	20	54	1.080	5.10	$0.135 \times 135 \times 135 = 2.60$	2φ14 = 3.08	3.52	0.57	6.5	13φ6
P18	360	375	420	1.100	-	2500	-	4.080	14.500	9.250	9.250	1	583.000	40	121	60	60	0.445	0.135	42	1600	$0.135 \times 135 \times 135 = 2.60$	3φ14 + 2φ12	5.470	20	54	1.080	5.10	$0.135 \times 135 \times 135 = 2.60$	2φ14 = 3.08	3.52	0.57	6.5	13φ6
P19	240	250	420	150	-	-	-	570	1370	685	685	1	81.000	35	68.5	24	21	0.485	0.156	49	1600	$0.156 \times 156 \times 156 = 3.65$	3φ10 + 1φ8	1.400	35	19	665	2.20	$0.156 \times 156 \times 156 = 3.65$	1φ8 + 1φ10 = 1.89	2.81	0.57	5	12φ6
P20	275	290	220	80	-	-	-	1.020	2.800	1.400	1.400	1/10	81.000	35	68.5	24	21	0.485	0.156	49	1600	$0.156 \times 156 \times 156 = 3.65$	3φ10	1.400	35	19	665	2.20	$0.156 \times 156 \times 156 = 3.65$	1φ10 = 0.79	2.41	0.57	5	10φ6
P21	240	250	220	800	-	-	-	1.020	2.800	1.400	1.400	1/10	81.000	35	68.5	24	21	0.485	0.156	49	1600	$0.156 \times 156 \times 156 = 3.65$	3φ10	1.400	35	19	665	2.20	$0.156 \times 156 \times 156 = 3.65$	1φ10 = 0.79	2.41	0.57	5	10φ6
P22	240	250	220	800	-	-	-	1.020	2.800	1.400	1.400	1/10	81.000	35	68.5	24	21	0.485	0.156	49	1600	$0.156 \times 156 \times 156 = 3.65$	3φ10	1.400	35	19	665	2.20	$0.156 \times 156 \times 156 = 3.65$	1φ10 = 0.79	2.41	0.57	5	10φ6
P23	325	340	220	680	-	-	-	900	2.900	1.450	1.450	1/10	99.000	36	57.5	24	21	0.400	0.170	51	1600	$0.170 \times 170 \times 170 = 5$	4φ10	1.450	36	19	665	2.30	$0.170 \times 170 \times 170 = 5$	2φ10 = 1.57	3.13	0.57	6	12φ6